**Preferred Device** 

# Power MOSFET 100 Amps, 100 Volts

## N-Channel TO-264

This advanced Power MOSFET is designed to withstand high energy in the avalanche and commutation modes. This new energy efficient design also offers a drain-to-source diode with fast recovery time. Designed for high voltage, high speed switching applications in power supplies, converters, PWM motor controls, and other inductive loads. The avalanche energy capability is specified to eliminate the guesswork in designs where inductive loads are switched and offer additional safety margin against unexpected voltage transients.

- Avalanche Energy Specified
- Diode is Characterized for Use in Bridge Circuits
- I<sub>DSS</sub> and V<sub>DS(on)</sub> Specified at Elevated Temperature

## MAXIMUM RATINGS (T<sub>C</sub> = 25°C unless otherwise noted)

Rating	Symbol	Value	Unit
Drain-Source Voltage	V <sub>DSS</sub>	100	Vdc
Drain-Gate Voltage ( $R_{GS} = 1 M\Omega$ )	V <sub>DGR</sub>	100	Vdc
Gate–Source Voltage  - Continuous  - Non–Repetitive (t <sub>p</sub> ≤ 10 ms)	V <sub>GS</sub> V <sub>GSM</sub>	±20 ±40	Vdc Vpk
Drain Current – Continuous @ $T_C$ = 25°C – Single Pulse ( $t_p \le 10 \mu s$ )	I <sub>D</sub> I <sub>DM</sub>	100 300	Adc Apk
Total Power Dissipation Derate above 25°C	P <sub>D</sub>	300 2.38	Watts W/°C
Operating and Storage Temperature Range	T <sub>J</sub> , T <sub>stg</sub>	-55 to 150	ů
Single Pulse Drain-to-Source Avalanche Energy – Starting $T_J = 25^{\circ}C$ ( $V_{DD} = 80$ Vdc, $V_{GS} = 10$ Vdc, Peak $I_L = 100$ Apk, $L = 0.1$ mH, $R_G = 25 \Omega$ )	E <sub>AS</sub>	250	mJ
Thermal Resistance – Junction to Case – Junction to Ambient	$R_{ hetaJC} \ R_{ hetaJA}$	0.42 40	°C/W
Maximum Lead Temperature for Soldering Purposes, 1/8" from case for 10 seconds	TL	260	°C



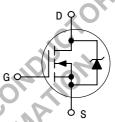
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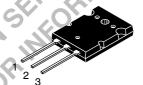
http://onsemi.com

# 100 AMPERES 100 VOLTS

 $R_{DS(on)} = 11 \text{ m}\Omega$ 

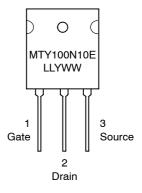






TO-264 CASE 340G Style 1

# MARKING DIAGRAM & PIN ASSIGNMENT



LL = Location Code Y = Year WW = Work Week

#### **ORDERING INFORMATION**

Device	Package	Shipping
MTY100N10E	TO-264	25 Units/Rail

**Preferred** devices are recommended choices for future use and best overall value.

## **ELECTRICAL CHARACTERISTICS** ( $T_J = 25^{\circ}C$ unless otherwise noted)

Cha	racteristic	Symbol	Min	Тур	Max	Unit
	racteristic	Cymbol	141111	196	WILL	Oint
OFF CHARACTERISTICS  Drain-Source Breakdown Voltage		V <sub>(BR)DSS</sub>				
$(V_{GS} = 0, I_D = 250 \mu A)$		(BR)DSS	100	_	_	Vdc
Temperature Coefficient (Positiv	e)		-	115	-	mV/°C
Zero Gate Voltage Drain Current		I <sub>DSS</sub>			4.0	μAdc
$(V_{DS} = 100 \text{ Vdc}, V_{GS} = 0 \text{ Vdc})$ $(V_{DS} = 100 \text{ Vdc}, V_{GS} = 0 \text{ Vdc}, T$	ı = 125°C)		_	_	10 200	
Gate-Body Leakage Current (V <sub>GS</sub>		I <sub>GSS</sub>	_	_	100	nAdc
ON CHARACTERISTICS (Note 1)	, 53 ,	400				
Gate Threshold Voltage		V <sub>GS(th)</sub>				
(V <sub>DS</sub> = V <sub>GS</sub> , I <sub>D</sub> = 250 μAdc) Threshold Temperature Coefficie	ent (Negative)	- 63(11)	2.0	- 7	4 –	Vdc mV/°C
Static Drain-Source On-Resistance		R <sub>DS(on)</sub>		_	0.011	Ohm
Drain-Source On-Voltage (V <sub>GS</sub> =		V <sub>DS(on)</sub>			0	Vdc
(I <sub>D</sub> = 100 Adc) (I <sub>D</sub> = 50 Adc, T <sub>J</sub> = 125°C)		Do(on)	_ _	1.0	1.2 1.0	
Forward Transconductance (V <sub>DS</sub> =	6 Vdc, I <sub>D</sub> = 50 Adc)	9FS	30	49	_	mhos
DYNAMIC CHARACTERISTICS		7	4	0,	4	•
Input Capacitance		C <sub>iss</sub>	7-8	7600	10640	pF
Output Capacitance	$(V_{DS} = 25 \text{ Vdc}, V_{GS} = 0 \text{ Vdc},$ f = 1  MHz)	C <sub>oss</sub>	CD.	3300	4620	
Reverse Transfer Capacitance	1 = 1 (VII 12)	C <sub>rss</sub>	1 - 1	1200	2400	
SWITCHING CHARACTERISTICS	(Note 2)	05 00	P			l
Turn-On Delay Time		<sup>‡</sup> d(on)	O,	48	96	ns
Rise Time	$(V_{DD} = 50 \text{ Vdc}, I_D = 100 \text{ Adc},$	t <sub>r</sub>	_	490	980	
Turn-Off Delay Time	$V_{GS} = 10 \text{ Vdc},$ $R_G = 9.1 \Omega)$	t <sub>d(off)</sub>	-	186	372	
Fall Time	110,011	Z.Gr	-	384	768	
Gate Charge		Q <sub>T</sub>	_	270	378	nC
(See Figure 8)	$(V_{DS} = 80 \text{ Vdc}, I_{D} = 100 \text{ Adc},$	Q <sub>1</sub>	_	50	_	
	$V_{GS} = 10 \text{ Vdc}, ID = 100 \text{ Adc},$ $V_{GS} = 10 \text{ Vdc})$	$Q_2$	-	150	_	
		Q <sub>3</sub>	_	118	_	
SOURCE-DRAIN DIODE CHARAC	TERISTICS					
Forward On-Voltage	C	$V_{SD}$				Vdc
, and the second	$(I_S = 100 \text{ Adc}, V_{GS} = 0 \text{ Vdc})$ $(I_S = 100 \text{ Adc}, V_{GS} = 0 \text{ Vdc}, T_J = 125^{\circ}\text{C})$	OD .	-	1	1.2	
	(35)	_	-	0.9	_	
Reverse Recovery Time (See Figure 14)		t <sub>rr</sub>	_	145	_	ns
	(I <sub>S</sub> = 100 Adc, V <sub>GS</sub> = 0 Vdc,	t <sub>a</sub>	-	90	_	
	$dI_{S}/dt = 100 \text{ A}/\mu\text{s})$	t <sub>b</sub>	=	55	=	
Reverse Recovery Stored Charge		Q <sub>RR</sub>	_	2.34	_	μС
INTERNAL PACKAGE INDUCTANO	DE					
Internal Drain Inductance (Measured from the drain lead 0	.25" from package to center of die)	L <sub>D</sub>	-	4.5	_	nH
Internal Source Inductance (Measured from the source lead	0.25" from package to source bond pad)	L <sub>S</sub>	-	13	-	nH
` 1 Pulse Test: Pulse Width <⅓00 us			<u> </u>	1		<u> </u>

Pulse Test: Pulse Width ≤300 μs, Duty Cycle ≤ 2%.
 Switching characteristics are independent of operating junction temperature.

#### TYPICAL ELECTRICAL CHARACTERISTICS

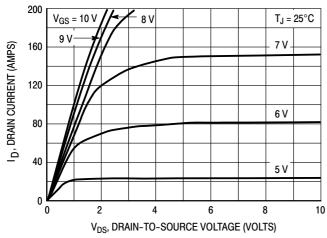


Figure 1. On-Region Characteristics

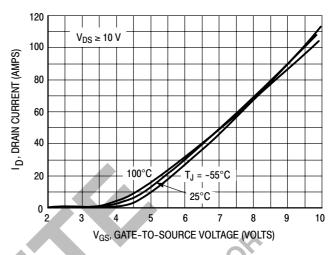


Figure 2. Transfer Characteristics

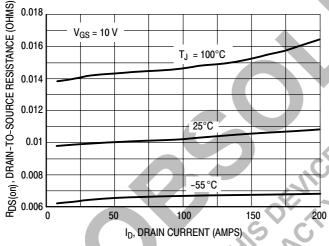


Figure 3. On-Resistance versus Drain Current and Temperature

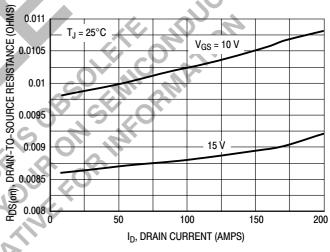


Figure 4. On-Resistance versus Drain Current and Gate Voltage

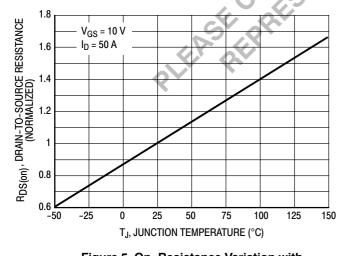


Figure 5. On–Resistance Variation with Temperature

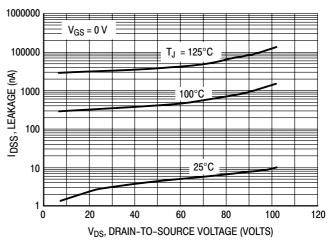


Figure 6. Drain-To-Source Leakage Current versus Voltage

#### POWER MOSFET SWITCHING

Switching behavior is most easily modeled and predicted by recognizing that the power MOSFET is charge controlled. The lengths of various switching intervals ( $\Delta t$ ) are determined by how fast the FET input capacitance can be charged by current from the generator.

The published capacitance data is difficult to use for calculating rise and fall because drain–gate capacitance varies greatly with applied voltage. Accordingly, gate charge data is used. In most cases, a satisfactory estimate of average input current ( $I_{G(AV)}$ ) can be made from a rudimentary analysis of the drive circuit so that

$$t = Q/I_{G(AV)}$$

During the rise and fall time interval when switching a resistive load,  $V_{GS}$  remains virtually constant at a level known as the plateau voltage,  $V_{SGP}$ . Therefore, rise and fall times may be approximated by the following:

$$t_r = Q_2 x R_G/(V_{GG} - V_{GSP})$$

$$t_f = Q_2 \times R_G/V_{GSP}$$

where

 $V_{GG}$  = the gate drive voltage, which varies from zero to  $V_{GG}$   $R_G$  = the gate drive resistance

and Q<sub>2</sub> and V<sub>GSP</sub> are read from the gate charge curve.

During the turn-on and turn-off delay times, gate current is not constant. The simplest calculation uses appropriate values from the capacitance curves in a standard equation for voltage change in an RC network. The equations are:

$$t_{d(on)} = R_G C_{iss} In \left[ V_{GG} / (V_{GG} - V_{GSP}) \right]$$

$$t_{d(off)} = R_G C_{iss} In (V_{GG}/V_{GSP})$$

The capacitance ( $C_{iss}$ ) is read from the capacitance curve at a voltage corresponding to the off-state condition when calculating  $t_{d(on)}$  and is read at a voltage corresponding to the on-state when calculating  $t_{d(off)}$ .

At high switching speeds, parasitic circuit elements complicate the analysis. The inductance of the MOSFET source lead, inside the package and in the circuit wiring which is common to both the drain and gate current paths, produces a voltage at the source which reduces the gate drive current. The voltage is determined by Ldi/dt, but since di/dt is a function of drain current, the mathematical solution is complex. The MOSFET output capacitance also complicates the mathematics. And finally, MOSFETs have finite internal gate resistance which effectively adds to the resistance of the driving source, but the internal resistance is difficult to measure and, consequently, is not specified.

The resistive switching time variation versus gate resistance (Figure 9) shows how typical switching performance is affected by the parasitic circuit elements. If the parasitics were not present, the slope of the curves would maintain a value of unity regardless of the switching speed. The circuit used to obtain the data is constructed to minimize common inductance in the drain and gate circuit loops and is believed readily achievable with board mounted components. Most power electronic loads are inductive; the data in the figure is taken with a resistive load, which approximates an optimally snubbed inductive load. Power MOSFETs may be safely operated into an inductive load; however, snubbing reduces switching losses.

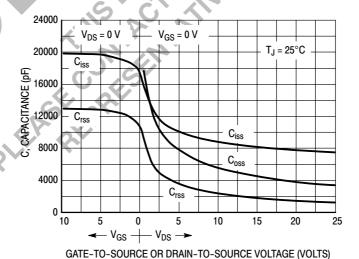


Figure 7. Capacitance Variation

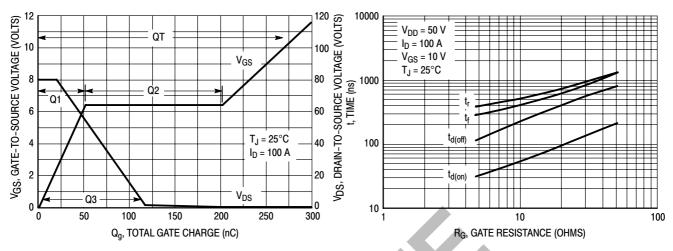


Figure 8. Gate Charge versus Gate-to-Source Voltage

Figure 9. Resistive Switching Time Variation versus Gate Resistance

## DRAIN-TO-SOURCE DIODE CHARACTERISTICS

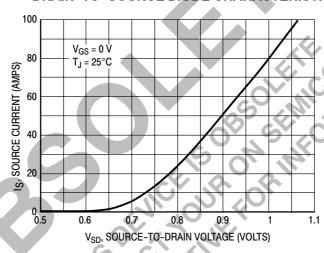


Figure 10. Diode Forward Voltage versus Current

### SAFE OPERATING AREA

The Forward Biased Safe Operating Area curves define the maximum simultaneous drain–to–source voltage and drain current that a transistor can handle safely when it is forward biased. Curves are based upon maximum peak junction temperature and a case temperature ( $T_{\rm C}$ ) of 25°C. Peak repetitive pulsed power limits are determined by using the thermal response data in conjunction with the procedures discussed in AN569, "Transient Thermal Resistance–General Data and Its Use."

Switching between the off-state and the on-state may traverse any load line provided neither rated peak current ( $I_{DM}$ ) nor rated voltage ( $V_{DSS}$ ) is exceeded and the transition time ( $t_r$ , $t_f$ ) do not exceed 10  $\mu$ s. In addition the total power averaged over a complete switching cycle must not exceed ( $T_{J(MAX)} - T_C$ )/( $R_{\theta JC}$ ).

A Power MOSFET designated E-FET can be safely used in switching circuits with unclamped inductive loads. For reliable operation, the stored energy from circuit inductance dissipated in the transistor while in avalanche must be less than the rated limit and adjusted for operating conditions differing from those specified. Although industry practice is to rate in terms of energy, avalanche energy capability is not a constant. The energy rating decreases non–linearly with an increase of peak current in avalanche and peak junction temperature.

Although many E-FETs can withstand the stress of drain-to-source avalanche at currents up to rated pulsed current ( $I_{DM}$ ), the energy rating is specified at rated continuous current ( $I_{D}$ ), in accordance with industry custom. The energy rating must be derated for temperature as shown in the accompanying graph (Figure 12). Maximum energy at currents below rated continuous  $I_{D}$  can safely be assumed to equal the values indicated.

#### SAFE OPERATING AREA

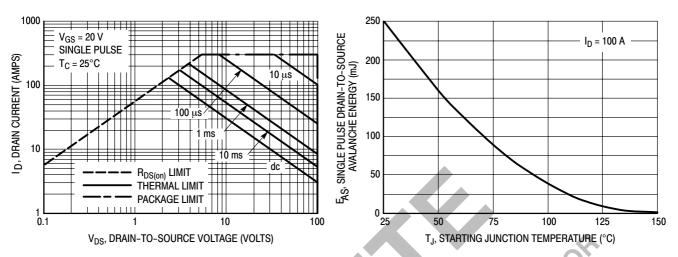
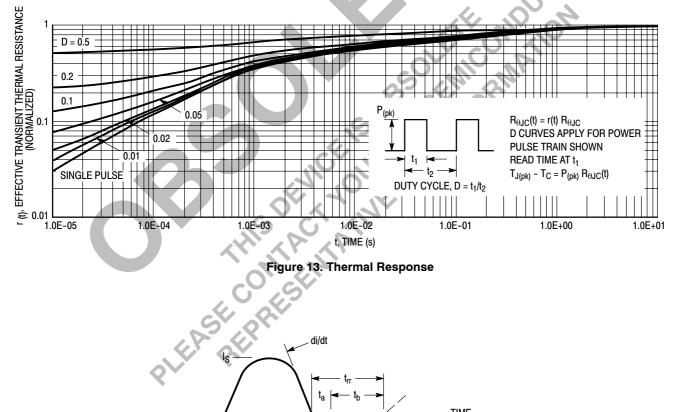


Figure 11. Maximum Rated Forward Biased **Safe Operating Area** 

Figure 12. Maximum Avalanche Energy versus **Starting Junction Temperature** 



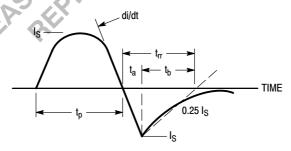
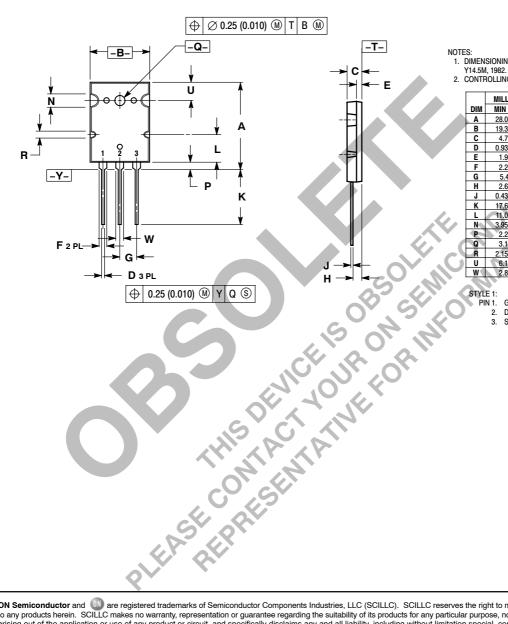


Figure 14. Diode Reverse Recovery Waveform

#### PACKAGE DIMENSIONS

TO-264 CASE 340G-02 **ISSUE H** 



#### NOTES:

- 1. DIMENSIONING AND TOLERANCING PER ANSI
- 2. CONTROLLING DIMENSION: MILLIMETER.

	MILLIMETERS		INCHES		
DIM	MIN	MAX	MIN	MAX	
Α	28.0	29.0	1.102	1.142	
В	19.3	20.3	0.760	0.800	
С	4.7	5.3	0.185	0.209	
D	0.93	1.48	0.037	0.058	
Е	1.9	2.1	0.075	0.083	
F	2.2	2.4	0.087	0.102	
G	5.45 BSC		0.215 BSC		
Н	2.6	3.0	0.102	0.118	
J	0.43	0.78	0.017	0.031	
K	17.6	18.8	0.693	0.740	
L	11.0	11.4	0.433	0.449	
N	3.95	4.75	0.156	0.187	
P	2.2	2.6	0.087	0.102	
D	3.1	3.5	0.122	0.137	
R	2.15	2.35	0.085	0.093	
O	6.1	6.5	0.240	0.256	
W	2.8	3.2	0.110	0.125	

DRAIN SOURCE

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